

AIAA 2003-4094

# Reliability Assessment of a Robust Design Under Uncertainty for a 3-D Flexible Wing

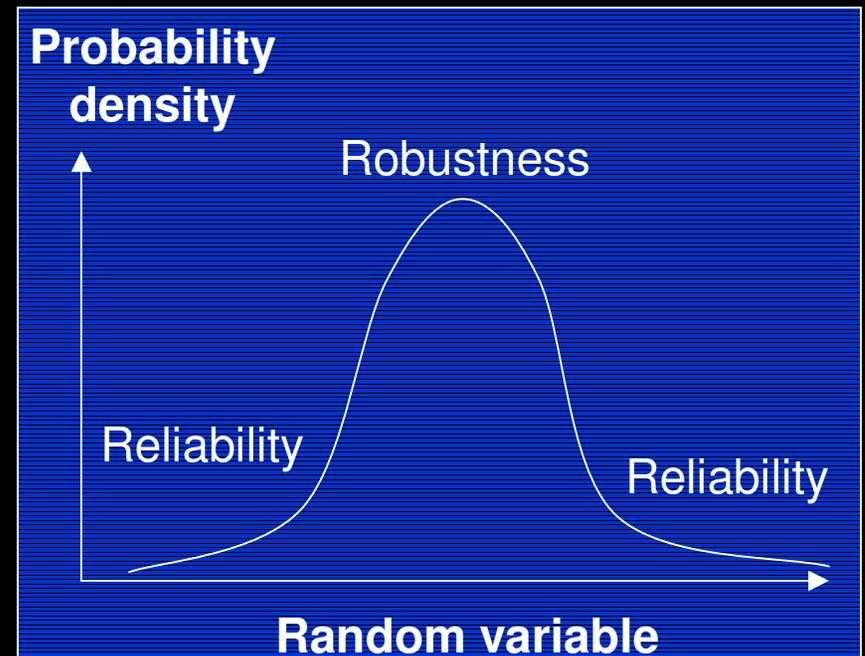
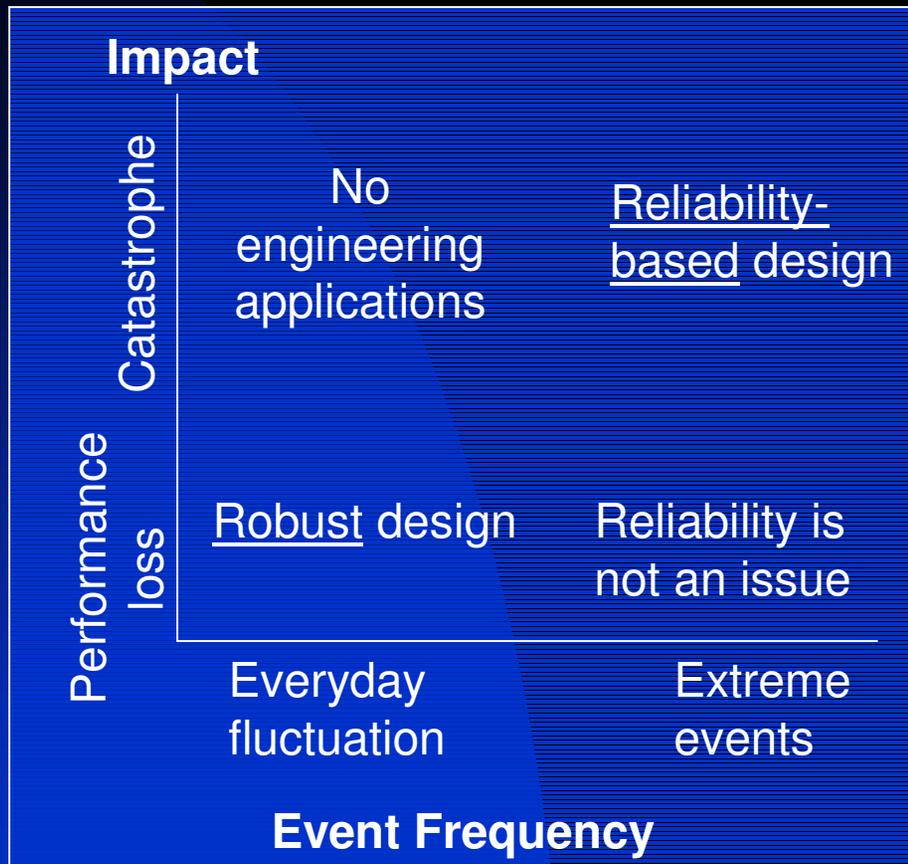
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# Uncertainty in Design



# Outline

- Robust Optimization method
- Reliability Analysis method
- Static aeroelastic wing optimization problem
- Reliability assessment of design points from Robust Optimization
- Assess suitability of Reliability Analysis for optimization

# First-Order Second Moment Approximation

- Random variables
  - ◆ statistically independent
  - ◆ normally distributed
  - ◆ with means  $\bar{b} = \{\bar{b}_1, \dots, \bar{b}_n\}$
  - ◆ and standard deviations  $\sigma = \{\sigma_1, \dots, \sigma_n\}$
- Expected values are

$$\bar{F} = F(\bar{b})$$
$$\sigma_F^2 = \sum_{i=1}^n \left( \frac{\partial F}{\partial b_i} \sigma_i \right)^2$$

# Robust Optimization

- Stochastic design variables
- Objective function cast as expected value of output function
- Constraints cast as a probability of satisfaction greater than  $\Phi(k)$

$$\begin{array}{ll} \min_{\bar{b}} & \Psi(\bar{F}, \sigma_F; \bar{Q}, \bar{b}) \\ \text{subject to} & g(\bar{F}; \bar{Q}, \bar{b}) + k\sigma_g \leq 0 \end{array}$$

- 2<sup>nd</sup> derivatives for gradient-based optimization

# Reliability Analysis (FORM)

$$u_i = \frac{b_i - \bar{b}_i}{\sigma_i}$$

■ PMA

$$\min_{\mathbf{u}} g(\mathbf{u})$$

subject to  $\sqrt{\mathbf{u}^T \mathbf{u}} - \beta_0 = 0$

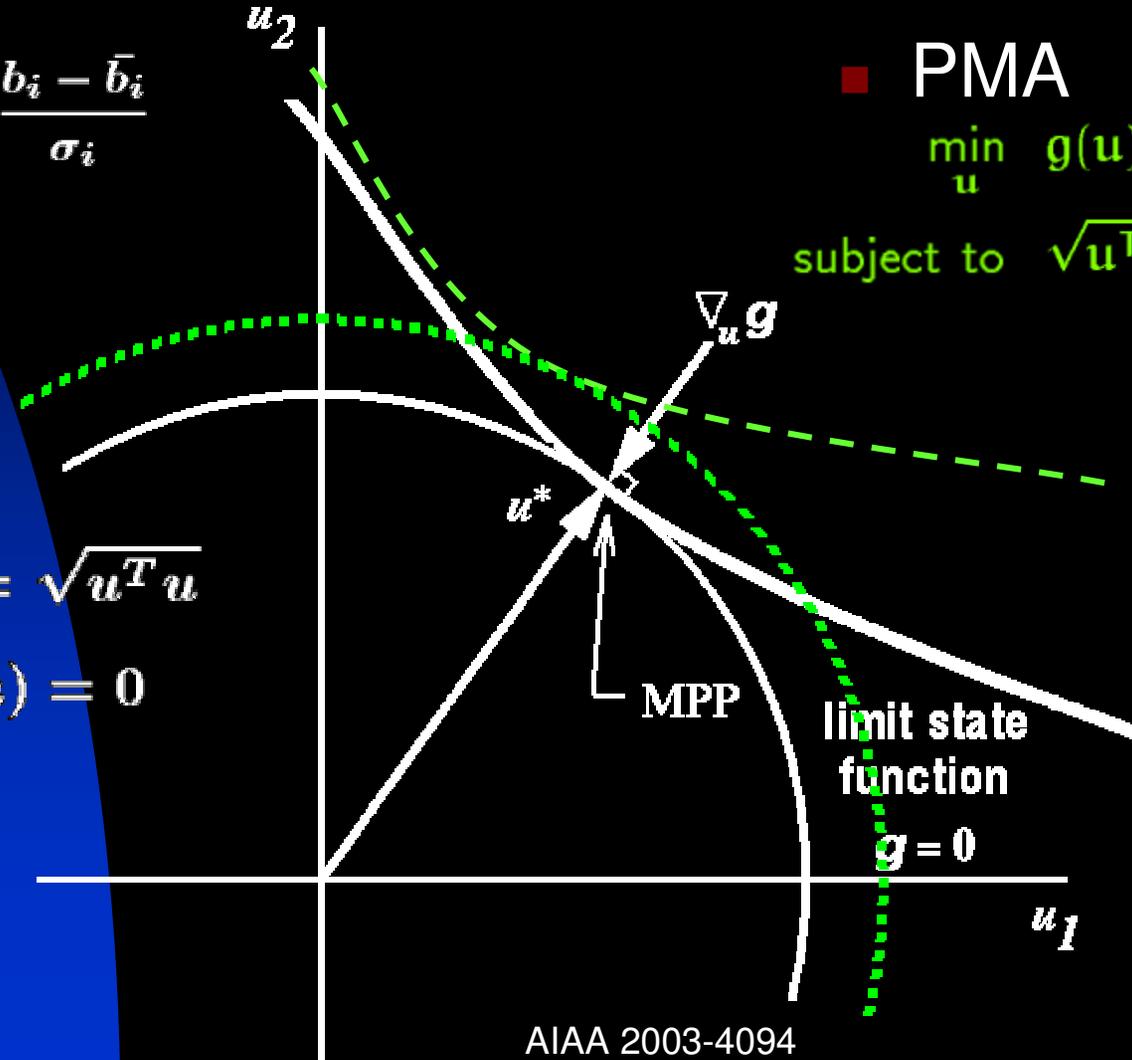
■ RIA

$$\min_{\mathbf{u}}$$

subject to

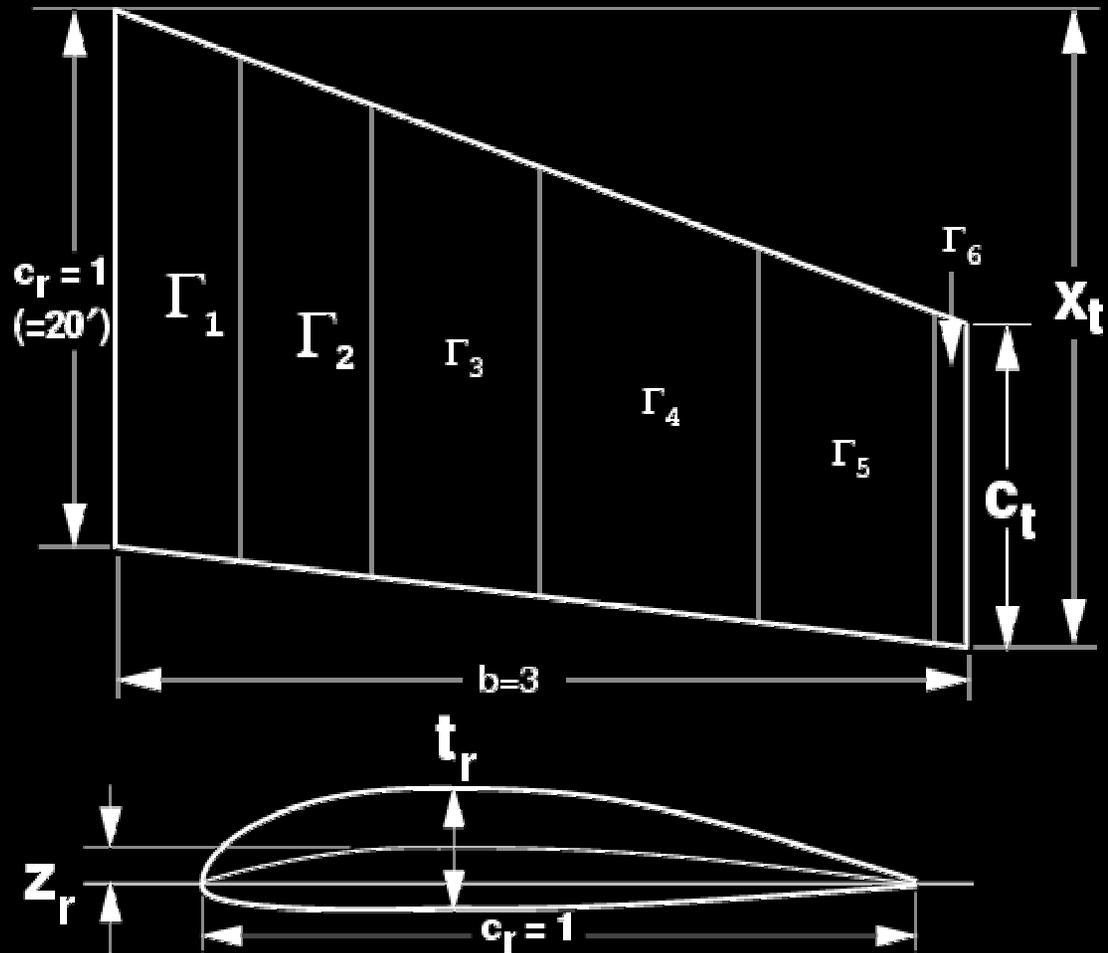
$$\beta = \sqrt{\mathbf{u}^T \mathbf{u}}$$

$$g(\mathbf{u}) = 0$$



# 3-D Flexible Wing

- Two DV
  - ◆  $C_t$ ,  $X_t$
- Four DV
  - ◆  $\Gamma_1, \Gamma_2$
  - ◆  $z_r, t_r$



# Objective and Constraints

■ Objective function:  $-(L/D)^2$

■ Constraints:

◆ Minimum payload  $L - W$

where  $L = C_L S q_\infty$

◆ Maximum compliance

$$V = \oint p u \cdot \hat{n} ds$$

◆ Maximum pitching moment  $C_m$

◆ Minimum LE radius

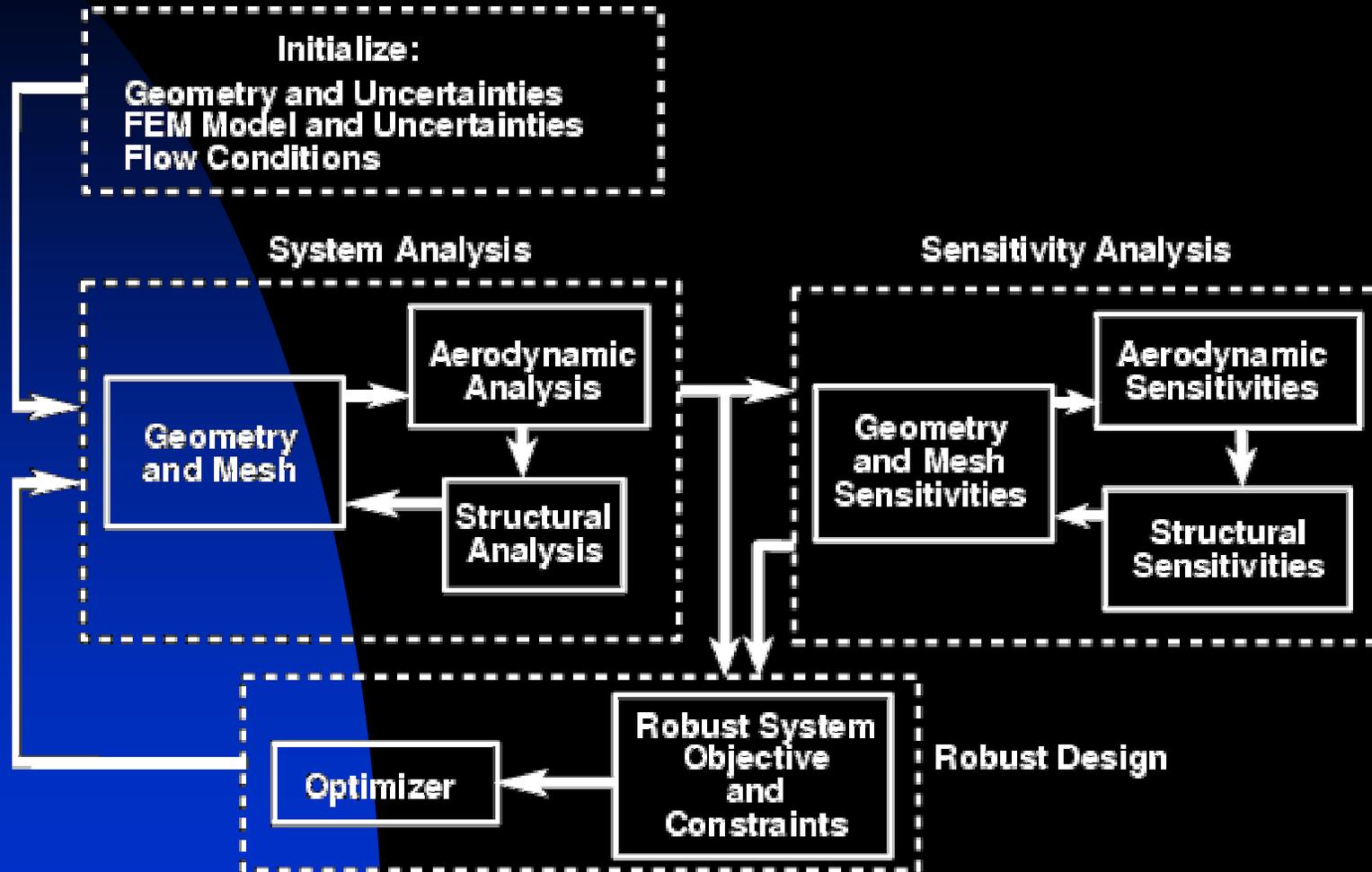
■ Solution of coupled Euler and FEM

analysis,  $R(Q,u,b)=0$ ,  $M_\infty = 0.8$ ,  $\alpha = 1^\circ$

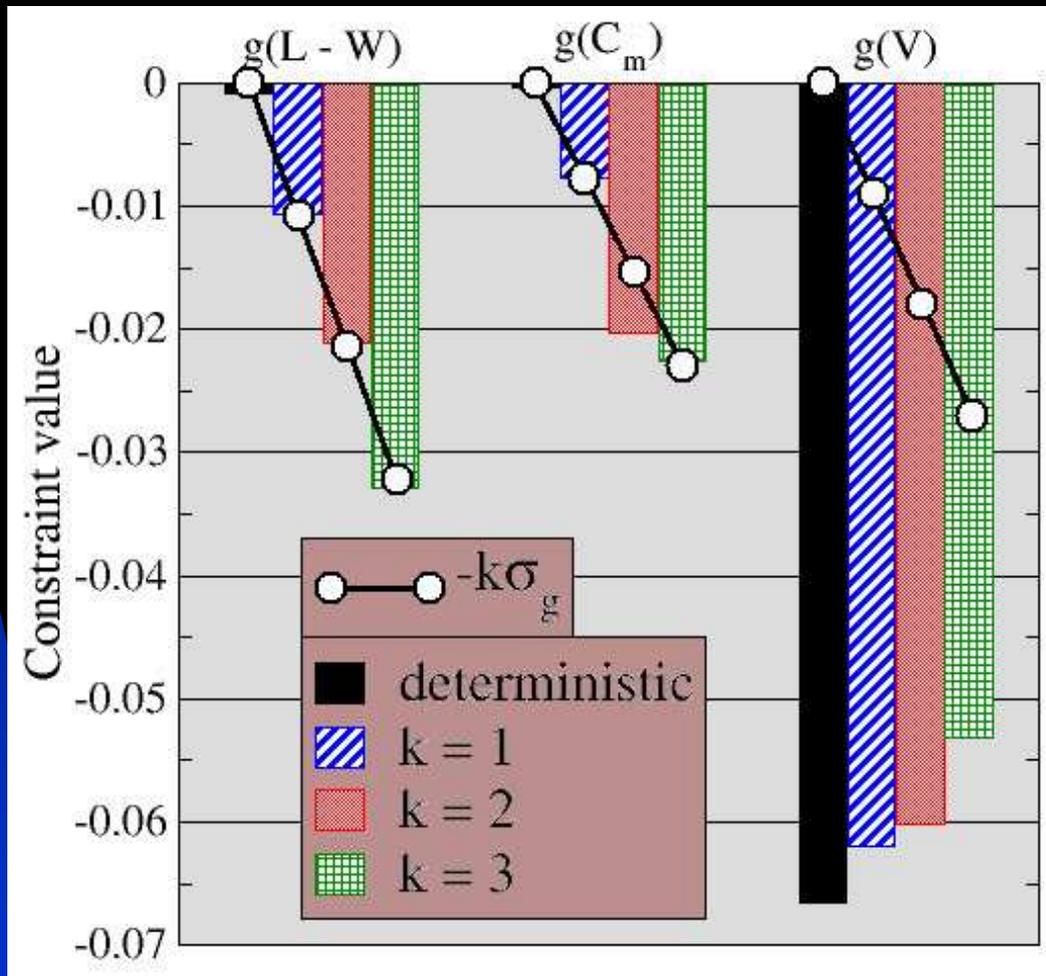
# Coupled CFD/FEM MDA

- Parameterized surface geometry
- Surface mesh deformation
- Volume mesh deformation
- 3-D Euler CFD
- Linear FEM: skin, spars, ribs
- Sensitivity analyses also coupled

# Optimization Process



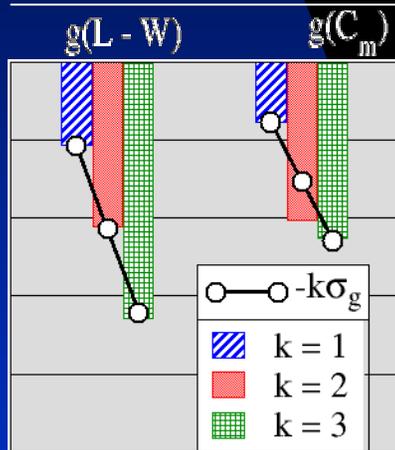
# Robust Results – 4DV



# Merit Functions for Reliability Assessment

Robust Design

$$g = \bar{g} + k\sigma_g \leq 0$$



$k$

$\bar{g} + k\sigma_g$

Reliability Analysis

$$P(g_p) = \Phi(-\beta)$$

$$\text{RIA: } g = 0 \Rightarrow \beta^*$$

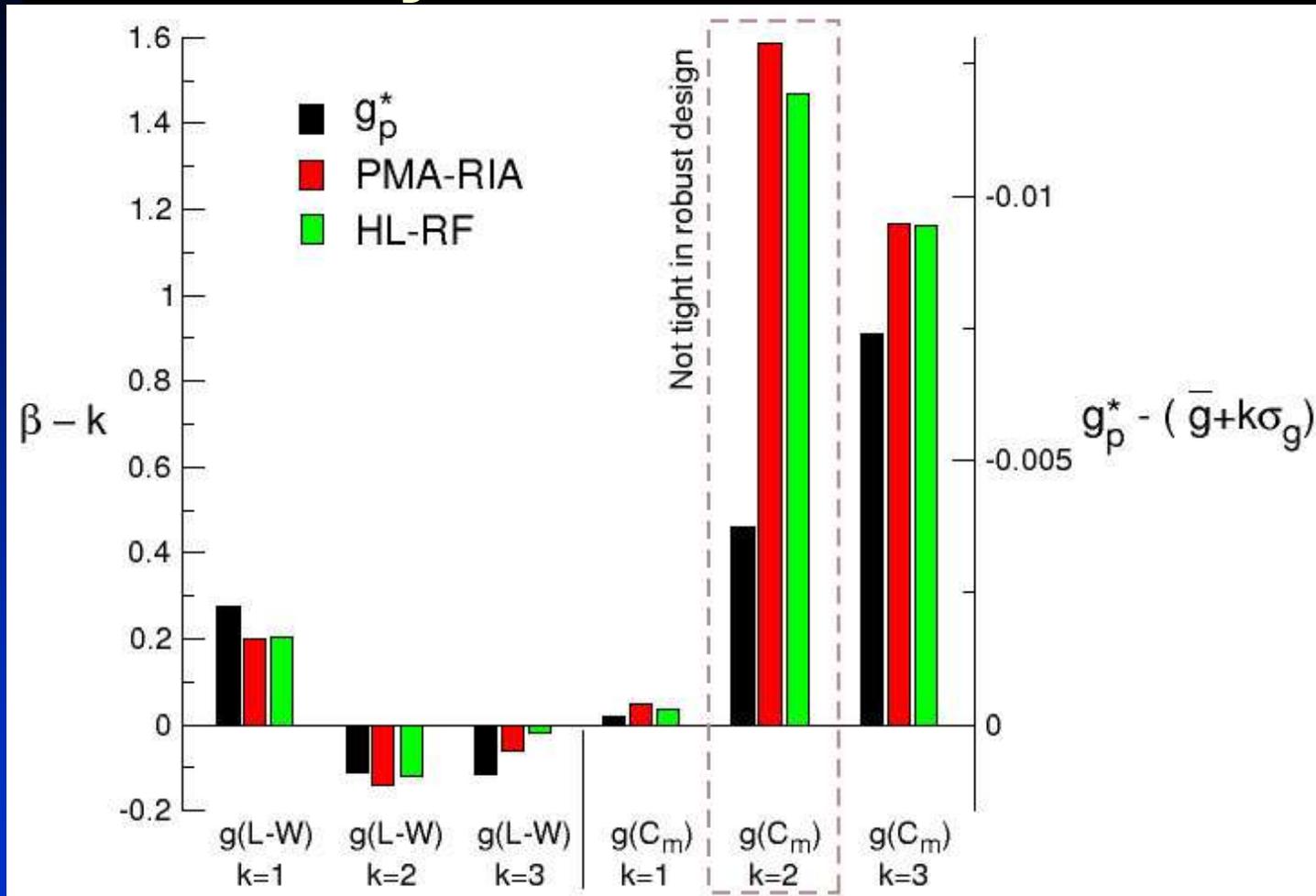
$$\text{PMA: } \beta_0 \Rightarrow g_p^*$$

Assessment functions:  
( near zero is good )

$$\beta^* - k$$

$$g_p^* - (\bar{g} + k\sigma_g)$$

# Reliability Assessment – 4DV



# Impact of Reliability Analysis on Optimization (RBDO)

- Inner optimization for RA
  - ◆ Required for each active constraint
  - ◆ Need screening process
- Sensitivity derivatives  $\frac{\partial \beta}{\partial DV}$  &  $\frac{\partial g^*}{\partial DV}$  required for gradient-based optimization
  - ◆ First derivative from inner optimization
  - ◆ Second derivative not required
- Accuracy and cost

# RA Sensitivity Derivatives – 4DV

DV	Constraint	k	$\frac{\partial \beta}{\partial DV}$ , HL-RF		$\frac{\partial \beta}{\partial DV}$ , PRIA		$\frac{\partial g^*}{\partial DV}$ , PMA	
			analytic	ratio	analytic	ratio	analytic	ratio
$\Gamma_1$	g(L – W)	1	-6.530	1.042	-6.530	1.004	.06952	0.992
$\Gamma_1$		2	-6.528	0.940	-6.527	1.008	.06917	0.998
$\Gamma_1$		3	-6.512	1.072	-6.511	1.011	.06881	0.998
$\Gamma_1$	g(C <sub>m</sub> )	1	-9.457	0.942			.05650	1.026
$\Gamma_1$		2	-9.778	†	-9.778	1.000	.05799	0.941
$\Gamma_1$		3	-9.984	†	-9.984		.05949	1.036
t <sub>r</sub>	g(C <sub>m</sub> )	3	-471.5		-471.5		2.802	1.008
z <sub>r</sub>		2	-818.4	†	-818.5	0.962	4.835	0.998
z <sub>r</sub>		3	-816.3		-816.3	0.990	4.846	1.000
$\Gamma_2$		2	-22.47	1.099	-22.47	0.958	.1332	0.999
$\Gamma_2$		3	-23.02	1.018	-23.02	1.003	.1372	0.991

† nonconvergent RIA for at least one side of the FD

# RA Cost Comparison

nDV	Constraint	k	HL-RF		PMA		PRIA	
			Nfunc	Nderiv	Nfunc	Nderiv	Nfunc	Nderiv
2	g(L-W)	1	3	3	3	3	6	5
2		2	3	3	3	3	6	5
2		3	3	3	3	3	6	5
2		4	5	5	3	3	10	8
2	g(V)	3	3	3	3	3	9	7
2		4			3	3	10	8
4	g(L-W)	1	3	3	3	3	6	5
4		3	3	3	3	3	6	5
4	g(C <sub>m</sub> )	1	4	4	3	3	6	5
4		2	3	3	3	3	6	5
4		3	3	3	3	3	9	7

# Summary & Conclusions

- Three reliability assessments more consistent with robust results at  $k \leq 3$
- PMA-based RIA eliminates non-convergence problem of HL-RF, but more expensive
- Reliability analysis derivatives suitable for RBDO
- Robust design requires second derivatives; reliability analysis requires additional optimization
- Use of PMA in design similar to Robust Design
- Use of PMA as screen for PRIA

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